

## Yaw stability regulation of electric vehicles based on model predictive control

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### Abstract

The yaw stability control system contributes significantly to the vehicle's lateral dynamics in order to enhance the vehicle's handling and stability. Controlling the lateral stability of a vehicle requires maintaining the proper yaw rate and side slip angle. For this purpose, a Model Predictive Control-based electric vehicle is built along with a stability control system. With a 2DOF vehicle model and a single track, the desired yaw rate is obtained. The controller is created using the Model Predictive Control (MPC) method. This controller modifies the steering angles of the front wheels and generates the necessary control moment for stabilizing the vehicle's yaw path. The stability control system and the developed controller are evaluated using a nonlinear single-track vehicle model, and the simulation results demonstrate improved vehicle performance and a good yaw rate compared to the vehicle's state without the controller.

**Keywords:** Vehicle Stability; Yaw Rate; Model Predictive Control

### 1. Introduction

Controlling the lateral dynamic motion of a road-vehicle is crucial for vehicle dynamic control, as it determines the vehicle's stability. A yaw stability control system is one of the primary systems published in the literature for lateral dynamics control. In order to construct an efficient control system, it is necessary to identify a suitable yaw stability control system component [1].

The lateral stability of the vehicle is a crucial performance that determines the vehicle's high-speed safety. The lateral dynamic performance is affected by numerous variables, such as the vehicle's structure, characteristics, starting operation, road conditions, tire steering angle, etc. Consequently, the design of the vehicle's lateral stability controller involved a complicated nonlinear problem. Recent research on the lateral stability of a vehicle included two factors: First, the research of vehicle lateral stability employs modern control theory and methods, such as model predictive control [2], sliding mode control [3], and so on, to use the yaw rate or slip angle as the controller's control parameters. The estimation of vital vehicle metrics and condition utilizing cutting-edge technology is another factor [4].

Some scholars propose control methods for vehicle stability and control, for example, Fuzzy PID control [5], Neural Network-Based Controller [6], traditional PID control method [7], Sliding Mode Control (SMC) [8], H/sub infinity / analysis and synthesis [9], Design of linear quadratic regulator (LQR) control [10], fractional-order PID control [11], and a hybrid LQR-PID control [12]. In addition to many other control methods available in research published in scientific journals and conferences.

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This study will develop a Simulink model of a vehicle stability system utilizing a model predictive controller and two vehicle models. The vehicle model utilized for this purpose will have seven degrees of freedom.

The study is structured as follows: in part II, the 7-DOF vehicle model represents the mathematical model of the actual vehicle. In the third section, the 2-DOF vehicle model is used for controller design and depicts the reference or desired model. In part IV, the control strategy demonstrates the complete Simulink model of the vehicle control system, whilst in section V, findings and simulation investigations of the yaw stability are shown to prove the superior tracking performance attained by utilizing a model predictive controller. In Section VI, conclusions are drawn.

## 2. Simulation models

This part of the paper shows two important models used in creating the control system of the vehicle, the first model is expressive of a 7 DOF model represents an actual vehicle, while the second model is 2 DOF model and is called the reference or bicycle model which to design of the controller and is also used to calculate the ideal reference yaw rate value.

### 2.1. Vehicle model

As depicted in Figure 1, the 7 DOF whole vehicle model includes the lateral, longitudinal, and yaw movements of the vehicle as well as the four-wheel movements. The vehicle's pitch, roll, and vertical movement were disregarded. Consequently, the longitudinal, lateral, and yaw movements of the vehicle, as well as the tire movement, were described as [13]:

The following describes the dynamic equations for the lateral, longitudinal, and yaw motions of the vehicle body.

- For yaw motion:

$$I \dot{Y}_r = L_1 (F_x^{fR} + F_x^{fL}) \sin \delta + L_1 (F_y^{fR} + F_y^{fL}) \cos \delta - L_2 (F_y^{rL} + F_y^{rR}) + \frac{D}{2} (F_x^{fR} - F_x^{fL}) \cos \delta + \frac{D}{2} (F_x^{rR} - F_x^{rL}) + \frac{D}{2} (F_y^{fL} - F_y^{fR}) \sin \delta \quad (1)$$

- For lateral motion:

$$\dot{v}_y + v_x Y_r = \frac{1}{m} [(F_y^{fL} + F_y^{fR}) \cos \delta + (F_y^{fR} + F_y^{fL}) \sin \delta + (F_x^{fR} + F_x^{fL}) \sin \delta + F_y^{rR} + F_y^{rL}] \quad (2)$$

- For longitudinal motion:

$$\dot{v}_x + v_x Y_r = \frac{1}{m} [(F_y^{fL} + F_y^{fR}) \cos \delta + (F_y^{fR} + F_y^{fL}) \sin \delta + (F_x^{fR} + F_x^{fL}) \sin \delta + F_y^{rR} + F_y^{rL}] \quad (3)$$

$F_y^{fL}, F_y^{fR}, F_y^{rL}, F_y^{rR}, F_x^{fR}, F_x^{fL}, F_x^{rR}, F_x^{rL}$  are the components of forces for the front left tire, front right tire, rear left tire, and the rear right tire along  $x$  axis  $y$  and axis coordinates;  $D$  is the displacement between left and right tires;  $a, b$  are the displacement of the COG of the vehicle to both of front and rear axle;  $v_x, v_y$  are the car longitudinal and the car lateral velocity,  $Y_r$  is the vehicle yaw rate,  $\delta$  is the front wheel steering angle,  $m$  is the vehicle total mass,  $I$  is the vehicle moment inertia about its yaw.  $F_x$  and  $F_y$  represent the tire forces, which will be determined using the Dugoff tire model.

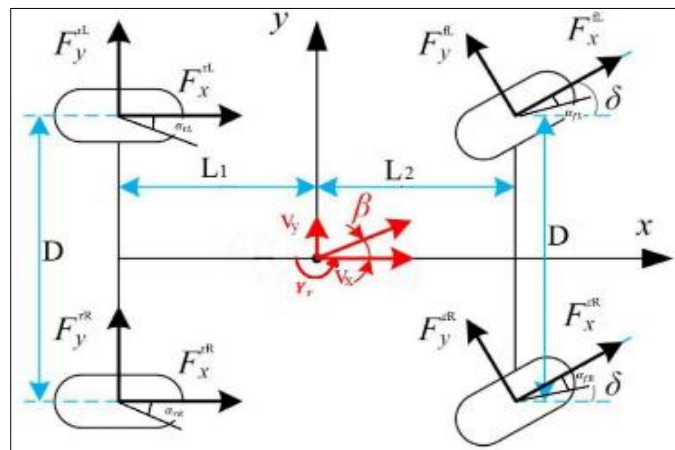


Figure 1 The Vehicle model.

### 2.2. 2 DOF vehicle model (Bicycle model)

In vehicle dynamic studies, the conventional 2 DOF vehicle model, often known as the bicycle model and seen in Figure 2, is widely used for yaw stability control analysis and controller design. This model is linearized from the nonlinear vehicle model on the basis of the following assumptions, which include:

- (1) Tire force ( $F_x$  and  $F_y$ ) operates in the linear region, (2) The vehicle moves on flat or plane road (planar motion), (3) Left and right wheels at the front and rear axles are lumped into a single wheel at the center line of the vehicle, (4) Constant vehicle speed i.e. the longitudinal acceleration equal to zero ( $a_x=0$ ), (5) Sideslip angle are assumed to be small ( $\beta \approx 0$ ), (6) No braking is applied at the two wheels, (8) Both front wheels have the same steering angle, and (9) desired vehicle sideslip is assumed to be zero in steady-state conditions.

The following equations represent the differential equations of lateral and yaw motions of the reference model:

$$mv(\dot{\beta}_d - Y_{rd}) = (F_y^f + F_y^r) - Y_{rd} \tag{4}$$

$$I_z \dot{Y}_{rd} = a \cdot F_y^f - b \cdot F_y^r \tag{5}$$

$$F_y^f = C_{af} \cdot \alpha_f \tag{6}$$

$$F_y^r = C_{ar} \cdot \alpha_r \tag{7}$$

$$\alpha_f = \delta - \beta_d - \frac{L_1 \cdot Y_{rd}}{v} \tag{8}$$

$$\alpha_r = -\beta_d + \frac{L_2 \cdot Y_{rd}}{v} \tag{9}$$

Where:

$Y_{rd}, \beta_d$  are the desired vehicle yaw rate and desired vehicle sideslip angle.

$C_{af}, C_{ar}$  are the longitudinal and the lateral stiffness of front wheel and rear wheel.

$L_1, L_2$  are the displacement of the COG of the vehicle to both of front and rear axle.

$\alpha_f, \alpha_r$  are the slip angle of front and rear tire.

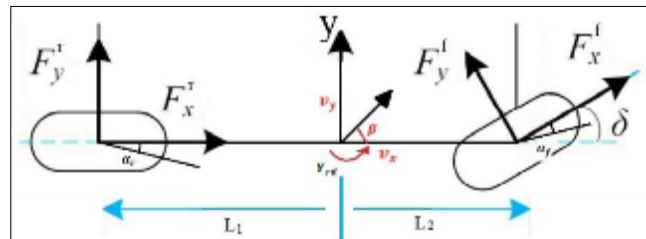


Figure 2 2 DOF vehicle model (Bicycle model)

In this model, the front and rear lateral tire forces  $F_y^f$  and  $F_y^r$  display linear characteristics and are characterized as a linear function of the front and rear cornering stiffness,  $C_1$  and  $C_2$ .

$$F_y^f = C_1 \cdot \alpha_f \tag{10}$$

$$F_y^r = C_2 \cdot \alpha_r \tag{11}$$

Where  $\alpha_f$  and  $\alpha_r$  are the sideslip angle at each wheel.

### 2.3. Dynamic response of vehicle model

MATLAB Simulink is used to analyze and simulate the previously mentioned vehicle model. It is presumed that the car is moving at an average speed of 70 km/h. In the simulations, the motorcar receives step and sinusoidal steering signals. The driver steering input for the step maneuver is shown in Figure 3. The step steering angle's amplitude is assumed to be 2 degrees (0.035 rad).

In the other case, the vehicle receives the sinusoidal steering input. The driver's steering input for the manoeuvre is shown in Figure 4. The peak value of the steering angle is assumed to be 2 degrees (0.035 rad).

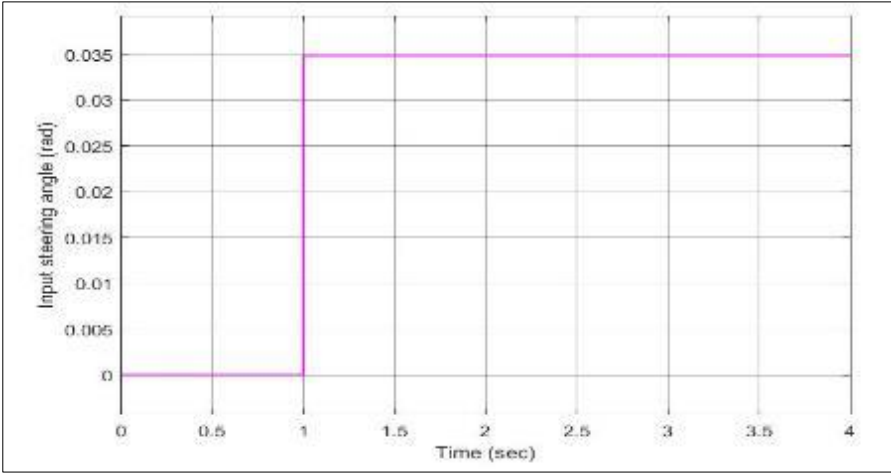


Figure 3 The steering input of vehicle maneuver

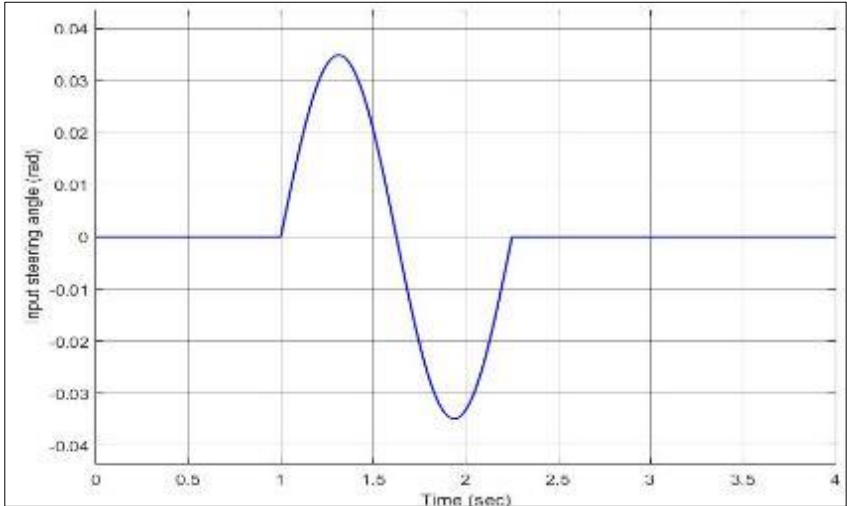


Figure 4 The steering input of vehicle with a lane change maneuver.

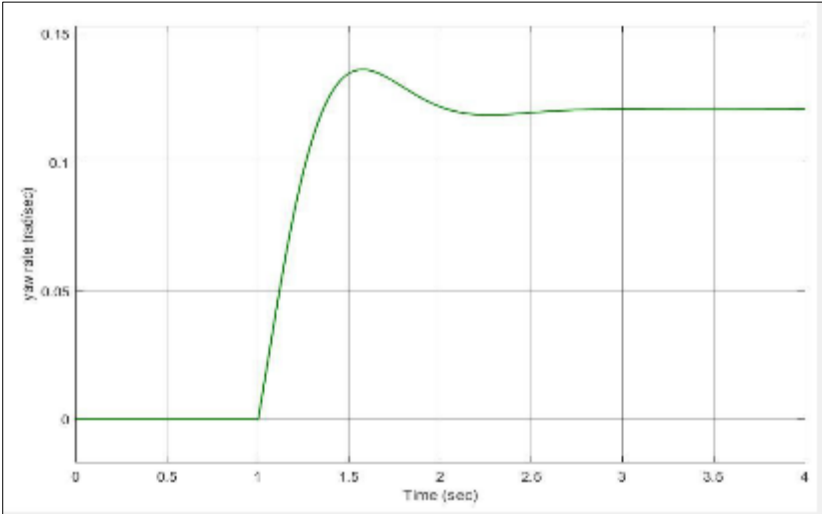
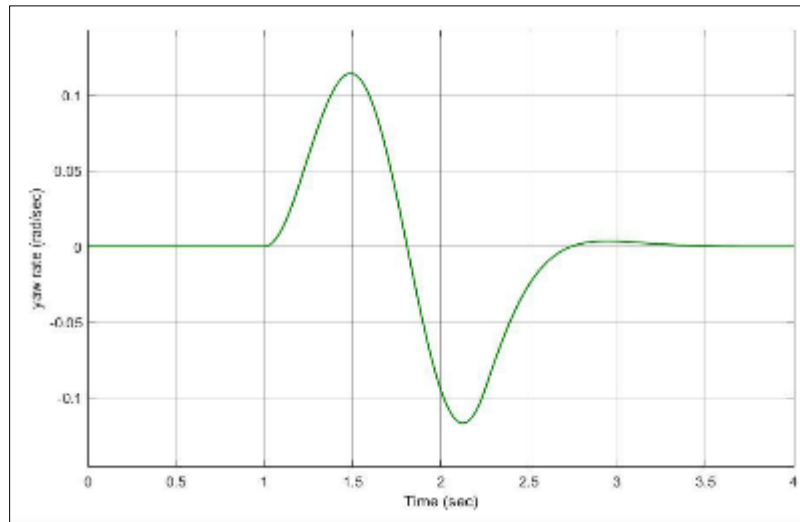


Figure 5 The vehicle yaw rate at a step signal of steering angle



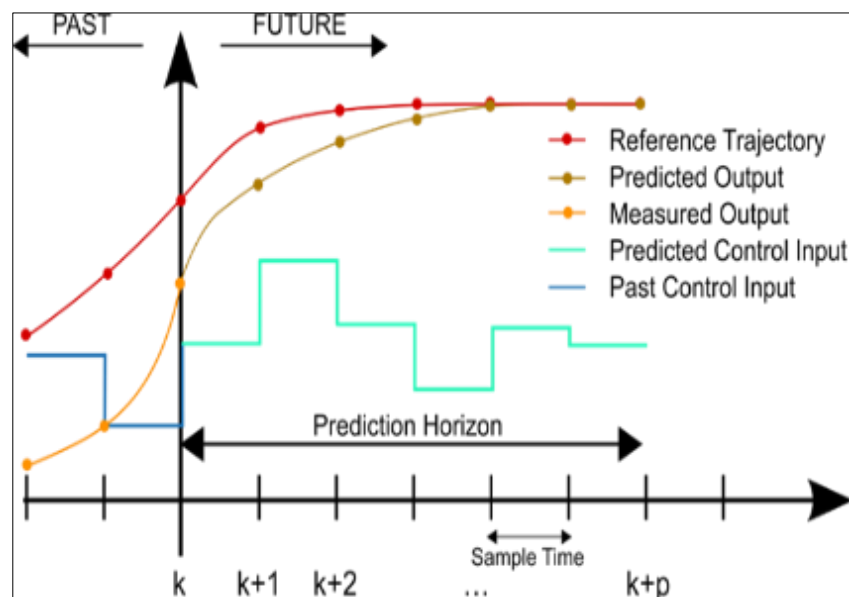
**Figure 6** The vehicle yaw rate on a lane change maneuver

In this paper, step and change of lane manoeuvres, as well as driving angle, will be used to measure and compare the vehicle's performance. This simulation produced the car's yaw rate performance for the passive scenario, which can be seen in Figures 5 and figure 6.

### 3. Model Predictive Control

An effective method for managing both linear and non-linear dynamic behavior of systems is the Model Predictive Controller (MPC), an advanced control system engineering technique. A Model Predictive Controller's (MPC) capability to handle multivariable dynamics and operational limitations effectively is its key advantage.

Figures 7 depicts the model predictive control block diagram and the fundamental notion of model predictive control with receding horizon control. It fits the following description of a strategy method: utilizing historical and current data to make predictions about the process output at a limited control horizon. Then, a control signal sequence is calculated by the optimizer taking into consideration the cost function and the constraints. The final step is performing the first control actions each time.



**Figure 7** Basic principle of model predictive controller

#### 4. Control techniques and strategies

In this paper, model predictive controller (MPC) is designed to enhance and improve the yaw stability of four-wheel drive vehicle. A control system is designed which includes three components: the Bicycle model reference vehicle model (reference vehicle model), planar model of the vehicle (A nonlinear model which represents actual vehicle), and the controller (MPC Controller). The structure of the control system of vehicle model with controller is illustrated in Figure 8.

A method for determining the ideal values of vehicle yaw rate and sideslip angle can be done using reference model and based on the steering angle ( $\delta$ ) which can be derived through the driver action.

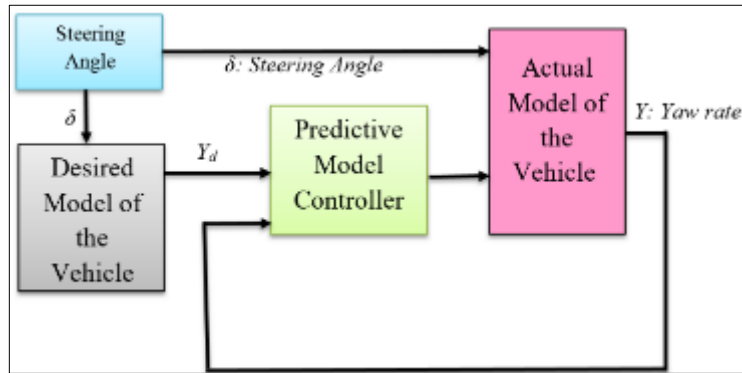


Figure 8 Vehicle control system Simulink structure

#### 5. Matlab simulations and discussion

As mentioned previously, in this paper the MPC controller was used, however we decided to compare the simulation results that resulted from the use of the MPC controller with the results of other simulations in which the traditional PID controller was used, where it was found that there was a slight difference in the results of the yaw rate and the sideslip angle when using the two controllers.

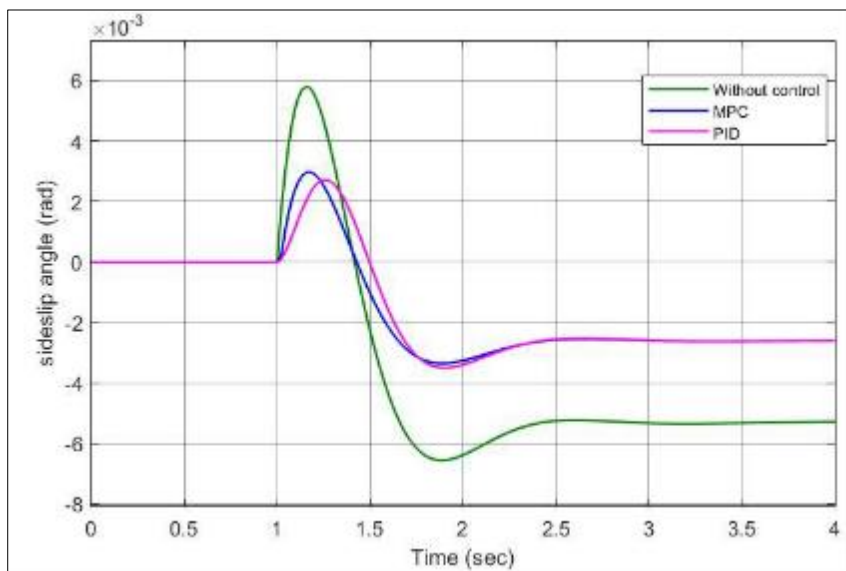
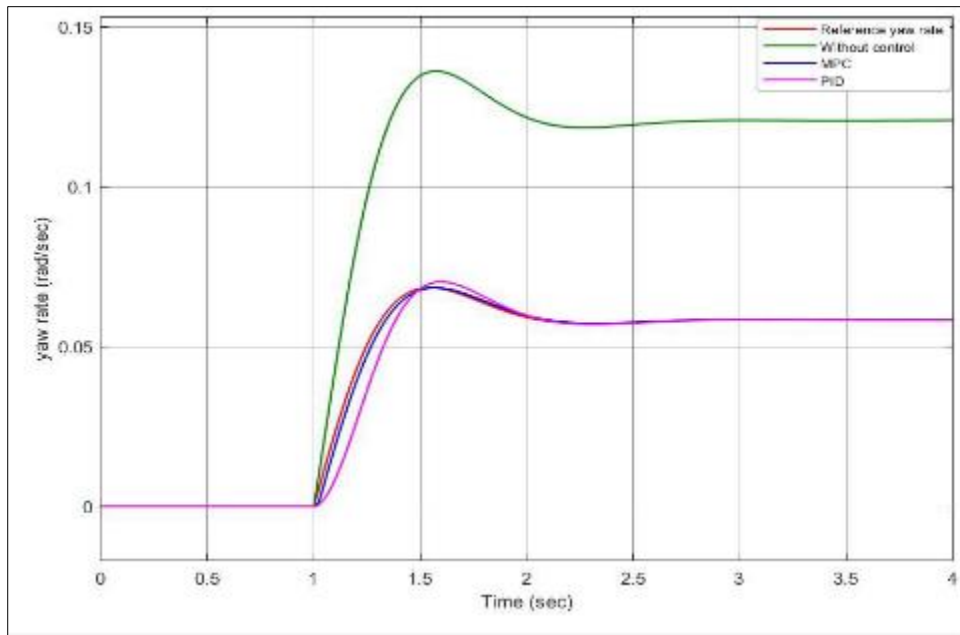


Figure 9 The vehicle sideslip angle at a step signal of steering angle

In order to evaluate the suggested controller system, two independent simulation experiments are carried out. a step steering angle was used for the initial simulation. The steering angle's amplitude is set to 2 degrees (0.035 rad), and the vehicle's speed is assumed to be 70 km/h.

The side slip angles are shown in Figure 9. The side slip angles of both controllers may be greatly reduced by steering the car's axles.

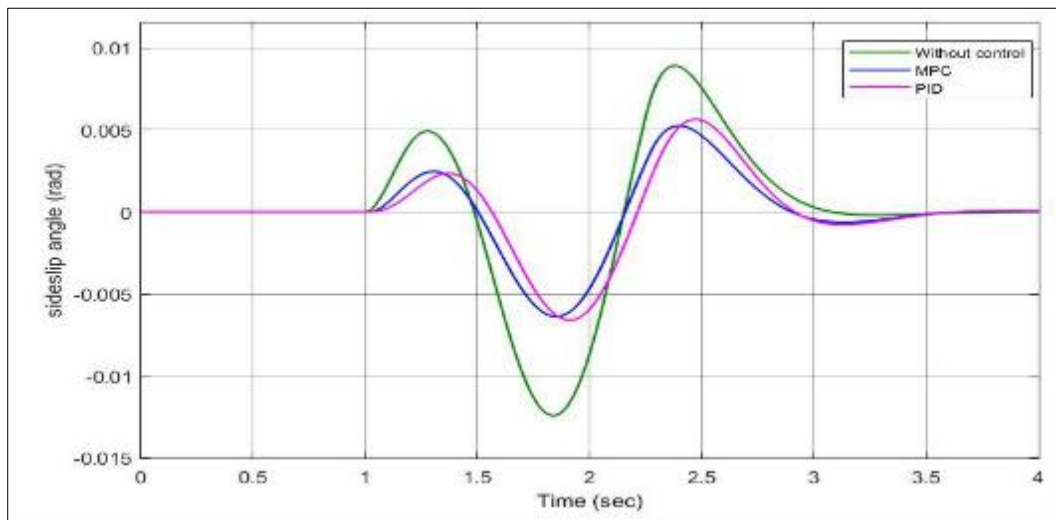
This simulation revealed differences in vehicle yaw rate for the passive and active scenarios, which can be observed in Figure 10. These results demonstrate that the controlled vehicle yaw rate response closely matches the planned yaw rate. Model predictive control is obviously more successful than PID in terms of effectiveness.



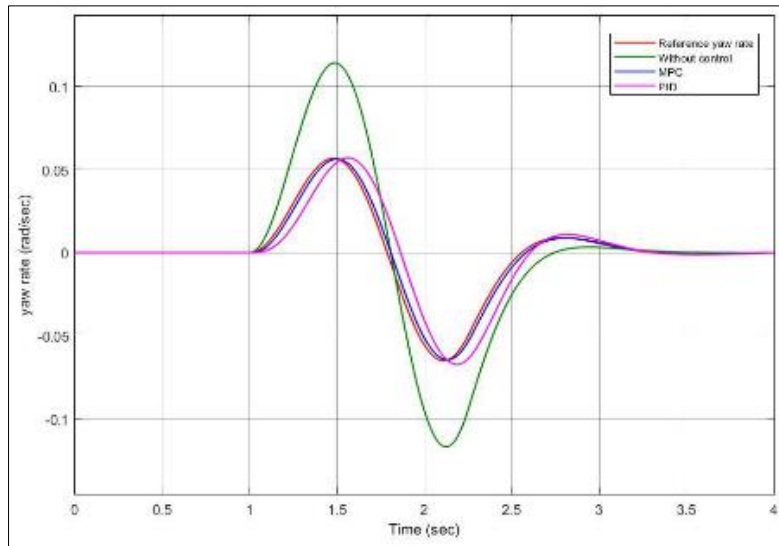
**Figure 10** The vehicle yaw rate behavior at a step signal of steering angle

The second simulation involves changing lanes maneuver. The steering input is set to a sinusoidal input with a 2 degrees (0.035 rad) amplitude.

Figure 11 and figure 12 demonstrate that the vehicle's yaw rate is nearly identical to the reference yaw rate. Furthermore, it is obvious that the side slip angle has gone down. Overall, the simulation findings show that all controllers, with the MPC controller preferred, are enhancing the lateral vehicle's performance.



**Figure 11** The vehicle sideslip angle on a lane change maneuver



**Figure 12** The vehicle yaw rate behavior on a lane change maneuver.

## 6. Conclusion

Aiming at improving the stability of vehicles and handling, the MATLAB Simulink model of the vehicle is implemented with MPC and PID controller to improve and ensure the vehicle yaw stability in this paper. To make sure this controller works well it has been tested at two scenarios of the input steering angle which are a step signal and a lane change maneuver. The results and plots show significant differences between the vehicle yaw rate and the vehicle body sideslip angle behaviors in the case when there is no control and the vehicle performance in the case with the model predictive controller. It is found that the yaw rate of the vehicle improved significantly, therefore, a vehicle control system constructed with MPC can achieve and enhance the required stability and performance of the vehicle. Also, it's noted that the Model predictive control is obviously more successful than the PID controller in terms of effectiveness.

## Compliance with ethical standards

### *Disclosure of conflict of interest*

The authors declare no competing interests.

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